

# Transverse profile expansion and homogenization at target for the injector Scheme- I test stand of China-ADS\*

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**Abstract:** For the injector Scheme- I test stand of the China-ADS (Accelerator Driven subcritical System), a beam with the maximum power of 100 kW will be produced and transported to the beam dump. To solve the very high thermal load problem at the dump, two measures are taken to deal with the huge power density at the target. One is to enlarge the contact area between the beam and the target, and this is to be accomplished by expanding the beam profile at the target and using slanted target plates. The other is to produce a more homogenous beam profile at the target to minimize the maximum power density. Here the beam dump line is designed to meet the requirement of beam expansion and homogenization at 3 different energies (3.2 MeV, 5 MeV and 10 MeV), and the step-like field magnets are employed for the beam spot homogenization. Taking into account the fact that the space charge effects are very strong at such low beam energies, the simulations have included space charge effects and errors which show that the beam line can meet the requirements very well. In the meantime, the alternative beam design using standard multipole magnets is also presented.

**Key words:** step-like field magnets, transverse profile expansion, transverse profile homogenization, beam line design

**PACS:** 29.27.Eg, 41.85.Ew **DOI:** 10.1088/1674-1137/39/2/027001

## 1 Introduction

The China-ADS (Accelerator Driven subcritical System) project is a strategic plan to solve the nuclear waste problem and the resource problem for nuclear power plants [1]. The driver accelerator runs in the continuous-wave mode and accelerates the 10 mA proton beam to 1.5 GeV to bombard the target to produce high-flux neutrons. Table 1 lists the main specifications. It can be seen that the ADS driver linac has very high beam power and very high reliability – qualities that are not possessed by any of the existing proton linacs in the world; innovative techniques must be applied. Among the R&D efforts, a test stand for the injector Scheme-I is being constructed at IHEP.

The test stand of the injector Scheme-I has a similar configuration to the formal one for the China-ADS [1], with the main difference being that the super conducting section is composed of two shorter cryomodules instead of a longer cryomodule in the formal design. It will be built and commissioned by steps. At the test stand, the accelerator will be able to produce a beam with the maximum power of 100 kW at 10 MeV. During the commis-

Table 1. Main specifications of the injector Scheme-I of China-ADS.

parameters	values
final beam energy/MeV	10
beam current/mA	10
beam duty factor (%)	100
RF frequency/MHz	325
beam power at target/kW	100
beam energy at the RFQ exit/MeV	3.2
beam energy at the 1st CM exit/MeV	5

ioning, the beam is transported to a high-power beam dump. By impinging the target at the beam dump, the beam power will be converted to thermal load and brought away by the cooling water. The target is composed of two copper plates welded together with 20° inclination angle, and then the contact area between the beam and target can be increased, hence the power density at the target surface can be lowered. Even so, it is still a big challenge if the 100 kW beam hits the target directly. Generally, the natural transverse beam distribution from a proton linac is more-or-less Gaussian, probably with a large beam halo. Similar to the other

Received 21 March 2014

\* Supported by CAS Strategic Priority Research Program- China-ADS and National Natural Science Foundation of China (11235012, 10975150)

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high beam power machines such as the European Spallation Source [2] and China Spallation Neutron Source (CSNS) [3], the dump beam line should be designed to expand and homogenize the transverse beam profile at the target. However, different from other applications using nonlinear magnets for beam spot homogenization at high beam energy where space charge effects can be ignored, here the space charge effects are strong due to very low beam energy and high beam current. In addition, the beam optics is very sensitive to errors at such low energy. Therefore, it is important to include the two effects in the studies.

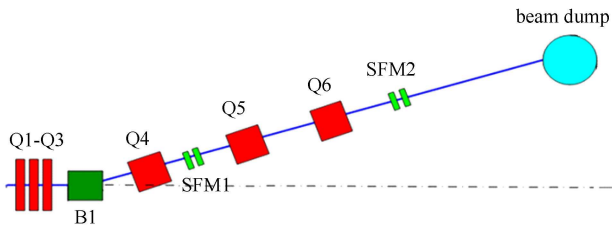


Fig. 1. Schematic layout of the beam dump line in the injector Scheme-I test stand of China-ADS.

## 2 Application of step-like field magnets for beam spot homogenization

Non-linear magnets, such as the standard multipole magnets, the step-like field magnets (SFM)[4] and the special multipole magnets [5], are usually required for the beam spot homogenization at the target. Due to its excellent properties of low beam loss, compactness and low cost, the SFMs are adopted here. As given in [3], one SFM will produce an anti-symmetric field with almost zero field in the centre and two flat-top fields with a sharp rise on the two sides. Two closely neighbouring SFMs with different designs will produce the required two-step field for the beam spot homogenization and for the beam halo control at the same time in one phase plane. This means that one needs at least two pairs of SFMs for the beam spot homogenization.

The step-like field distribution of an SFM can be expressed approximately by

$$B(x) = \frac{F_s/L}{1 + e^{-b(x-x_0)}}, \quad (1)$$

where  $L$  and  $x_0$  are the effective length and the step position respectively, both are almost fixed in the magnet design.  $F_s$  and  $b$  are the field strength and the step sharpness, which can be changed by adjusting the power supplies of the two independent coils and are used for the optimization of the beam spot homogenization during commissioning.

## 3 Design of the dump beamline

According to the multiple-phase development plan of the test stand, in the first phase the commissioning is focused on the RFQ with the beam energy of 3.2 MeV. In the second phase it is focused on the first superconducting section of 7 spoke cavities housed in the cryomodule CM1 with the beam energy of 5 MeV. In the third phase, it is focused on the second superconducting section which is identical to the first one and housed in the cryomodule CM2 with the beam energy of 10 MeV, as shown in Fig. 2. Therefore, the dump beam line has been designed to fit the beams with three different characteristics. As defined in [1], the dump beam line is a part of MEBT2, but here it transports beams at the 3 different energies of 3.2 MeV (RFQ exit), 5 MeV (CM1 exit) and 10 MeV (CM2 exit), respectively.

### 3.1 Design goals and constraints

The dump beam line is designed with the following guidelines:

(1) To facilitate the dump design which should be compact to fit in the existing tunnel, the transverse beam profile at the dump entrance should be more-or-less rectangular. The footprint ( $4\sigma \times 4\sigma$ ) is required to be not smaller than  $200 \text{ mm} \times 200 \text{ mm}$ ,  $141 \text{ mm} \times 141 \text{ mm}$  and  $110 \text{ mm} \times 110 \text{ mm}$  at 10 MeV, 5 MeV and 3.2 MeV respectively to make sure that the average beam power density in the transverse plane is lower than  $250 \text{ W/cm}^2$  at all the 3 energies. In the meantime, the peak power density is required to be less than  $585 \text{ W/cm}^2$ , which is determined by the  $200 \text{ W/cm}^2$  power density limit at the copper target surface and the  $20^\circ$  inclination angle.

(2) The homogeneity of the beam power density on the target should be as good as possible, which is determined by the design margin of the beam dump, about 10% in root-mean-square (rms) here.

(3) At the beam dump entrance or the so-called target, the beam halo outside of  $\pm 130 \text{ mm}$  in both the horizontal and vertical directions should be very low, e.g. less than 0.1% of the total beam power, as there is no cooling for the vacuum chamber which receives this part of the beam.

(4) For reasons of hands-on maintenance and device protection, the beam loss rate along the beam line should be controlled to be as low as possible. A total beam loss rate of a few tens Watts in the beam line is considered acceptable.

(5) The beam line should be designed to adopt different beam characteristics at the three different stages. The whole beam line and the beam dump will be reinstalled during the later stages. The devices remain the same but the relative positions can be adjusted slightly.

Although the beam energy is low, a few quadrupoles with quite large apertures are applied to produce very

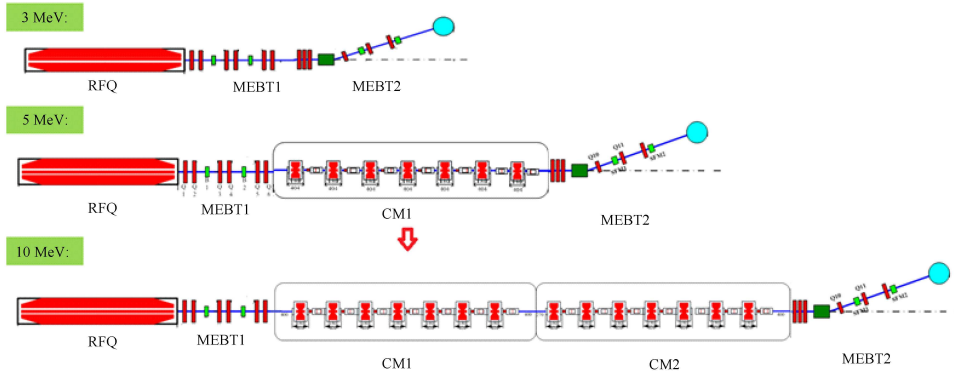


Fig. 2. Three stages of the construction and beam commissioning of the injector Scheme-I test stand of the China-ADS.

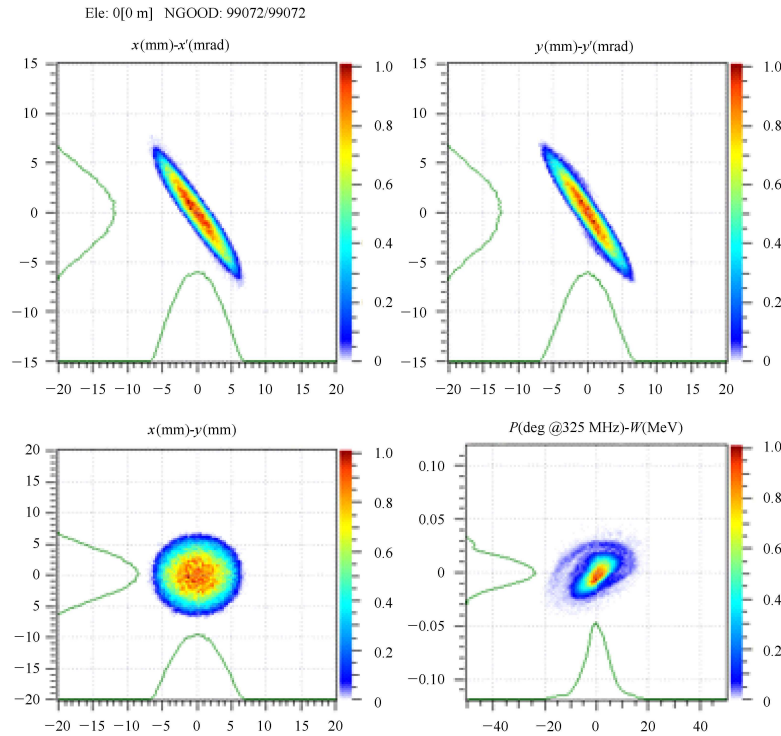


Fig. 3. Beam distributions in the phase spaces at the MEBT1 exit.

flat beams at the positions of the SFMs. The optimizations are made to reduce the requirements on the quadrupole strengths.

### 3.2 Design methods

As mentioned before, to control the beam homogeneity in both the horizontal and vertical planes, two pairs of SFMs are applied in the beamline. The aspect ratio of the beam cross-section at the SFMs should be large enough to decouple the nonlinear field in the two phase planes, e.g. larger than 6. At the same time, the phase advance between the SFMs and the target should be designed to be slightly different from  $\pi$  or  $2\pi$ . Thus, to adjust the beam optics flexibly, one needs at least four

quadruples, two of which are put before the first pair of SFMs, and the other two are located between the two pairs of SFMs.

A  $15^\circ$  bending magnet is introduced to avoid the back-streaming neutrons from the target entering the cryostats. Therefore, two more quadrupoles are used for the transverse focusing, as shown in Fig. 1.

TRANSPORT [6], TURTLE [7] codes are used to set up the preliminary beam optics without applying the SFMs, while the TraceWin [8] code is used to optimize the optics including space charge effects and the nonlinear fields of the SFMs. Usually, several iterations need to be carried out for the optimization of the linear optics and the SFMs. The element errors with orbit correction

are included in the simulations with TraceWin.

For the multi-particle trackings by TraceWin, different initial beam distributions for 3.2 MeV, 5 MeV and 10 MeV at the beam line entrance are from the injector beam dynamics design, which are initially based on the RFQ design and contain 99072 macro-particles at the RFQ exit.

### 3.3 At 3.2 MeV

At 3.2 MeV, the dump beamline is connected directly to MEBT1. Fig. 3 shows the beam phase space distribution at the MEBT1 exit. The linear beam optics for the dump beamline is shown in Fig. 4, which is designed to have flat beams at the SFMs and an enlarged beam profile at target with an initial emittance of  $15\pi\text{mm}\cdot\text{mrad}$  which contains 99% particles.

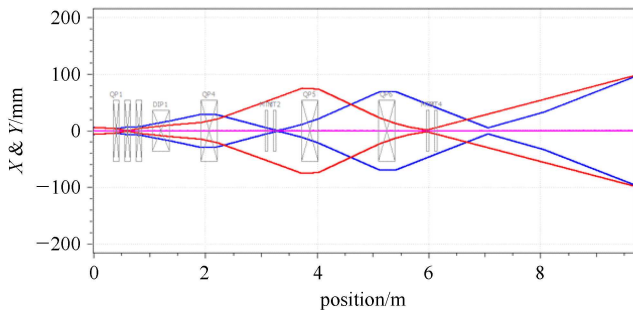


Fig. 4. Linear beam optics for the 3.2 MeV dump beam line.

The multi-particle tracking result at the target entrance is shown in Fig. 5. For comparison, the design result by using octupoles in the place of the SFMs was also carried out and shown in the figure, whose homogeneity looks slightly worse at target. The rms homogeneity of the beam power density on the flat top is about 11% by using the SFMs, while it is about 19% for the case of octupoles. The maximum beam power density at target is  $246\text{ W/cm}^2$ , which is far below the design requirement. With the given total macro-particles, there

are statistical errors of a few percent in the homogeneity calculations that are due to relatively small numbers of macro-particles in each grid, and here  $6\text{ mm}\times 6\text{ mm}$  size grids are used. With the beam orbit correction, the error simulations show that no beam loss is observed for the case of SFMs.

### 3.4 At 5 MeV and 10 MeV

At higher beam energy, the beam emittance is smaller, while the required magnetic fields for the bending magnets, the quadrupole magnets and the SFMs are higher. In order to obtain a better control on the beam halo and the beam loss at both 5 MeV and 10 MeV, the 2nd pair of SFMs is moved upstream by 0.3 m from the setup at 3.2 MeV.

Although they all meet the design goals, it is found that at 5 MeV it gives the best results on the beam halo control and the transverse profile homogeneity, compared with the cases at 3.2 MeV and 10 MeV. To control the homogeneity error contributed by the statistical errors, the size of the grids are changed to  $8\text{ mm}\times 8\text{ mm}$  at 5 MeV and  $10\text{ mm}\times 10\text{ mm}$  at 10 MeV to keep averaged macro-particles per grid almost the same for the 3 cases. The flat top homogeneity and the peak power of the beam power density at target are 11% in rms and  $320\text{ W/cm}^2$  at 5 MeV, 14% in rms and  $385\text{ W/cm}^2$  at 10 MeV. At 3.2 MeV, the performance is mainly limited by the relatively stronger space charge effect, while the main limitation for 10 MeV is the maximum magnetic field of the 3 large-aperture quadrupoles.

With the beam orbit correction, the average beam loss along the beam line is only several Watts at 5 MeV, and about 10 W at 10 MeV. This is considered acceptable at such low beam energy even though special treatments are required. Most of the beam loss happens between Q5 and Q6.

### 3.5 Simulations with 3D SFM field map

In the previous simulations, 2D SFM field maps are used. To check the performance with field maps as close

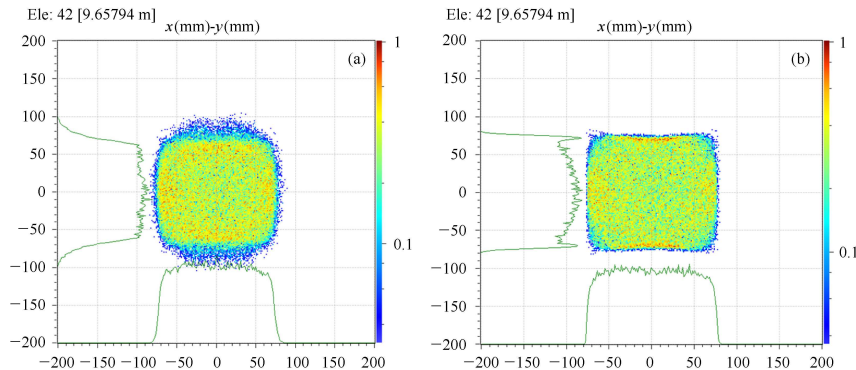


Fig. 5. Transverse beam profiles at the beam dump entrance at 3.2 MeV ((a) with SFMs; (b) with octupoles).

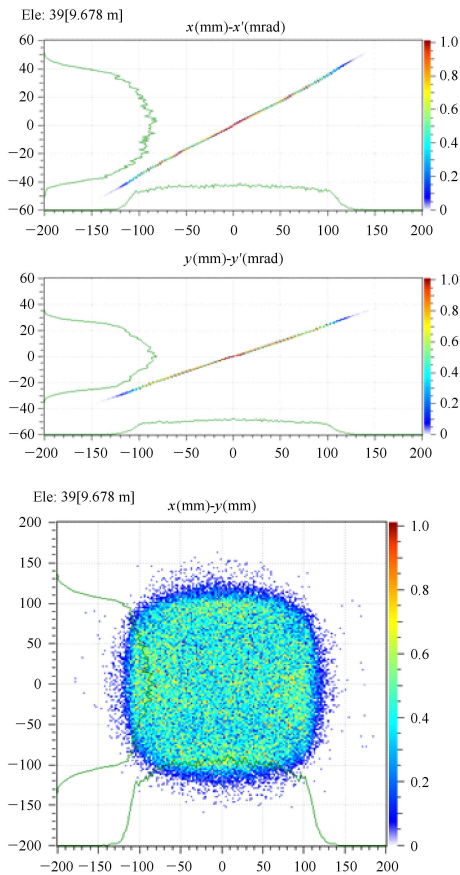


Fig. 6. Particle distribution in the transverse phase planes at the target at 10 MeV with the 3D SFM field maps.

Table 2. Beam losses along the beam line and the beam power distributions at the target.

	3 MeV	5 MeV	10 MeV
loss without errors/W	no loss	<2	<2
loss with errors/W	no loss	<5	<10
major loss positions		DCCT, FCT	B1, Q5-Q6
beam power out of footprint/W		55	267
beam power out of target/W		15	95
homogeneity across the flat top/(%, rms)	10	11	14
peak power density on target/(W/cm <sup>2</sup> )	246	320	385

to reality as possible, 3D SFM field maps are generated by OPERA [9]. Fig. 6 shows the beam profile at the target at 10 MeV. It looks as though the 3D result is only slightly worse than the 2D case, but still meets the design goal.

### 3.6 Summary of the designs

For all the 3 different energies, the beam losses along the beam line and the beam power distributions at the target are summarized in Table 2. The main design parameters for the magnets in the beam line are listed in Table 3.

Table 3. Main design parameters for the magnets in the dump beam line.

parameters	length/m	magnet field gradient (T/m)/strength (T)
Q1	0.1	0.98
Q2	0.1	6.59
Q3	0.1	11.30
Q4	0.3	2.56
SFMY-1	0.08	0.029
SFMY-2	0.08	0.05
Q5	0.3	1.76
Q6	0.3	1.90
SFMX-1	0.08	0.036
SFMX-2	0.08	0.16

## 4 Conclusions

To facilitate the commissioning of the injector Scheme-I for the China-ADS linac, a dump beam line together with the beam dump is designed, which uses the SFMs to produce homogenized beam footprints at the target. The beam dynamics simulations show that the designed beam line can work very well at 3 different energies (3.2 MeV, 5 MeV and 10 MeV), which meets the requirements on the beam profile at target and the beam losses in the beam line.

*The authors would like to thank all the colleagues in the China-ADS beam dynamics group for their very helpful discussions.*

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